ANALYSIS OF FEEDING MECHANISM IN MICROSTRIP PATCH ANTENNA

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Abstract
This paper presents a comparative design between microstrip and coaxial feeding mechanism used in microstrip patch antenna along with the optimization of resonant frequency, return loss, Antenna impedance, VSWR, Gain etc. The Full wave analysis simulation is carried out in HFSS tool in the frequency range of 2-3 GHz i.e. in S band for Wi-fi application.

Keywords— Microstrip patch Antenna, Microstrip feeding, Coaxial feeding, Simulation Results.

1. INTRODUCTION
The patch antenna was first proposed in the early 1950s but it was not used until 1970s when this type of antenna attracted main attention in commercial and defense purpose. Today Microstrip antenna is most widely used antenna because of its low cost, light weight, ease of fabrication, printed technology, conformable to planner and non planner surfaces, feed line and impedance matching network can be integrated, but having some drawbacks also like low gain and narrow impedance bandwidth typically less than 5%, low efficiency, low power, High Q factor (greater than 100), poor polarization purity and spurious feed radiation[1,2]. In the high performance aircraft, space craft, missiles and satellites where size, cost, weight, performance, aerodynamics profile are constraints, a low profile antenna is required.

By increasing the height of substrate, we can increase the Bandwidth and Radiation efficiency but at the same time the surface waves comes in pictures which travel within the substrate and they scattered at the bends and surface discontinuity, at the truncation of dielectric and ground plane. This extracts the power from total available power, hence decreases the efficiency. The surface waves can be eliminated by using the cavity. By the Stacking method we can increase the Bandwidth. The matching between the Patch antenna and feed network is mainly depends on the feeding technique used for this. The substrate height should be of the order of 0.003 < h < 0.05 of λ to reduce the surface waves [3].

For the Coplanar application the microstrip feed is directly connected to the edge of the patch and coaxial feed is used otherwise. The position of feed point controls the impedance matching condition. The cross polarization is due to the undesired higher order modes generated in patch and is affected because of both electrical and geometrical parameters. Patch array provides much higher gain than a single patch antenna element so they are usually used in airplane and military applications. A wireless LAN is used as an extension to, or an alternative to the wired LAN. A single patch antenna provides a gain from 6-9 dBi[4-22].

2. MICROSTRIP FEEDING TECHNIQUE
In the Microstrip feeding technique, the feed line is quarter wavelength long which is used for the impedance matching between the 50Ω line impedance and the Patch Antenna impedance. This is easy to fabricate. Impedance matching is simple by controlling insert feed position. The spurious radiation is low (nearly -20 dB) and have narrow bandwidth (1-5%).

Fig 1: Microstrip feed Patch Antenna

The figure (1) shows the basic microstrip feed patch structure, having Length is equal to half of the resonating wavelength which is matched with 50 ohm line through microstrip feed and Figure (2) represents the equivalent representation of microstrip feed. The feed contributes the inductive part to the patch.
3. DESIGN PROCEDURE OF PATCH ANTENNA

In the Transmission line Model of Patch Antenna, the two slots are placed at half wavelength apart and the fringing field distribution is extended at length $\Delta L$ [1].

$$\Delta L = 0.412h \left( \frac{\varepsilon_{eff} + 0.3}{\varepsilon_{eff} - 0.258} \right) \left( \frac{W}{h} + 0.264 \right) \left( \frac{W}{h} + 0.8 \right)$$

The effective Dielectric constant is given by

$$\varepsilon_{eff} = \frac{\varepsilon_r + 1}{2} + \frac{\varepsilon_r - 1}{2 \sqrt{1 + \frac{12h}{W}}}$$

Width of Patch is:

$$W = \frac{c}{2f_o \sqrt{\varepsilon_r + 1}}$$

Hence the effective length of Patch is given by:

$$L_{eff} = L + 2\Delta L$$

Where,

$$L_{eff} = \frac{c}{2f_o \sqrt{\varepsilon_{eff}}}$$

The input impedance of Patch is

$$Z_o = 90 \frac{\varepsilon_r^2}{\varepsilon_r - 1} \left( \frac{L}{W} \right)^2$$

The width of the Quarter wave line is given by:

$$Z_t = \frac{60}{\sqrt{\varepsilon_r}} \ln \left( \frac{8d + \frac{8}{w_t}}{\frac{w_t}{4d}} \right)$$

Where $Z_t$ is calculated as: $Z_t = \sqrt{50*Z_o}$

The length of Quarter line is $L_t = \frac{\lambda}{4} = \frac{\lambda_0}{4\sqrt{\varepsilon_{eff}}}$

The width of 50Ω line is given by:

$$Z_o = \frac{120\pi}{\sqrt{\varepsilon_r [1.393 + \frac{W}{h} + \frac{2}{3} \ln(\frac{W}{h} + 1.444)]}}$$

4. COAXIAL PROBE FEEDING TECHNIQUE

In the coaxial line feed, the inner conductor of the coax penetrates the substrate from the back of the ground plane without any contact with the ground plane by making a hole in it and is attached to the radiating patch, while the outer conductor is connected to the ground plane. Hence the coupling mechanism is purely inductive in nature. Spurious radiation is low (nearly -50 dB) and bandwidth is also narrow (1-5%). This is rejected in the space mission because possibly it may break during the launching because of vibrations.

Radius of central conductor = 0.63mm
Radius of inner dielectric(Teflon($\varepsilon_r$=2.1))=2.25mm
Radius of outer conductor = 2.5mm

The figure(3) shows a coaxial feeding to the microstrip patch where the inner conductor connected with patch while the outer conductor touches the ground plane. The location of feed point is selected to the patch so that it gives the best impedance match with 50Ω line. The central conductor is in direct contact with the patch while the rest of part is behind the ground. Hence it minimizes the spurious radiation but the main drawback is that it's not easy task to model the equivalent of probe using the EM tools. Thicker substrates can increase the surface waves and high cross polarized fields. The impedance matching is that point on the patch from the centre where we are getting a 50 Ω impedance and this can be calculated since we know the impedance at the corner of patch. We are using the dielectric material RT Duroid of dielectric constant of 2.2. Impedance at $y=y_0$ from Patch edge is given as[1]:

$$R(y = y_0) = R(y = 0) \cos^2 \left( \frac{\pi y}{L} \right)$$

While the impedance of coaxial line is as:
The main advantage of coaxial probe feed is fabrication and matching is easy, and it has low spurious radiation. But, it has problem of narrow bandwidth and more difficult to model, mainly for thick substrates.

\[
Z = \frac{60}{\sqrt{\varepsilon_r}} \ln\left(\frac{b}{a}\right)
\]

The figure (4) shows the equivalent circuit of coax feed patch where \( L_c \) denotes the inductive part due to inner conductor.

**Fig 4:** Equivalent circuit of coaxial Patch Antenna

5. SIMULATION AND RESULTS

**Table 1** - The design Parameters of Microstrip Patch

<table>
<thead>
<tr>
<th>Design Parameters</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Operating frequency ( f_o )</td>
<td>2.4 GHz</td>
</tr>
<tr>
<td>substrate height ( h )</td>
<td>1.57mm</td>
</tr>
<tr>
<td>dielectric constant ( \varepsilon_r )</td>
<td>2.2</td>
</tr>
<tr>
<td>thickness of metal ( t )</td>
<td>35 µm</td>
</tr>
</tbody>
</table>

5.1 Microstrip Feed Patch

Using the formula given above, we can find the Patch dimensions which are designed in HFSS.

**Table 2** - Dimension the Patch antenna

<table>
<thead>
<tr>
<th>Dimension of Patch Antenna</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Width of patch</td>
<td>41.08 mm</td>
</tr>
<tr>
<td>Length of patch</td>
<td>40.55 mm</td>
</tr>
<tr>
<td>Length of Quarter line</td>
<td>24.05 mm</td>
</tr>
<tr>
<td>Width of Quarter line</td>
<td>0.52 mm</td>
</tr>
<tr>
<td>Length of 50 Ω line</td>
<td>15 mm</td>
</tr>
<tr>
<td>Width of 50 Ω line</td>
<td>4.84 mm</td>
</tr>
</tbody>
</table>

This figure (a) shows the Microstrip feed patch structure implemented on HFSS.

This figure (b) the return loss of patch in dB with respect to the frequency. This helps to calculate the impedance bandwidth.

This figure (c),(d) shows the gain of the patch in the Boreside direction and another figure shows the smith chart plot w.r.t. the frequency.
This figure (e), (f) shows the Real and imaginary part of impedance variation w. r. t. to the frequency. The net impedance should be 50 ohm for the best match and the good return loss.

This figure (g), the E field variation in the azimuth plane of the patch and HPBW can be calculated from this.

This figure (h), the radiation efficiency plot of patch antenna.

This figure (i), gives the variation of the surface current density on the patch antenna. We can see that the current is maximum at the centre while its zero at the edges.

**Fig 5:** (a) Circuit diagram of Microstrip feed (b) Return loss (c) Gain (d) Smith Chart (e) Re (Impedance) Plot (f) Im (Impedance) Plot (g) Radiation pattern of E at phi = 0 deg. (h) Antenna Radiation Efficiency (i) Surface Current density on Patch

**5.2 COAXIAL PROBE FEED PATCH**

In the coaxial feed patch antenna, the position of feed is taken as 6.22 mm from the centre of the patch where the feed impedance is equal to 50Ω.
This figure (a) shows the Coaxial feed patch structure implemented on HFSS.

![Figure (a)](image1)

This figure (b) shows the return loss of patch in dB with respect to the frequency. This helps to calculate the impedance bandwidth.

![Figure (b)](image2)

This figure (c), (d) shows the gain of the patch in the Boreside direction which shows a gain of 7.157 dB and another figure shows the smith chart plot w.r.t. the frequency.

![Figure (c)](image3) ![Figure (d)](image4)

This figure (g), the E field variation in the azimuth plane of the patch and HPBW can be calculated from this.

![Figure (g)](image5)

This figure (h), the radiation efficiency plot of patch antenna

![Figure (h)](image6)

![Figure (i)](image7)
This figure (i), gives the variation of the surface current density on the patch antenna. It represents the magnitude variation. We can see that the current is maximum at the centre while its zero at the edges.

**Fig 6:** (a) Circuit diagram of Coaxial feed (b) Return loss (c) Gain (d) Smith Chart (e) Re (Impedance) Plot (f) Im (Impedance) Plot (g) Radiation pattern of E at phi = 0 deg. (h) Antenna Radiation Efficiency (i) Surface Current density on Patch

6. APPLICATION

This patch antenna is used for Wifi, WLAN application at 2.4 GHz frequency for narrow band operation. Since we have used the low dielectric constant material for the fabrication of patch hence the radiation efficiency is good. We can introduce the reconfigurability in our design hence this can be used for two different frequency applications using the same patch antenna.

7. CONCLUSIONS

**Table 3-** Comparison in the Two feeding Techniques

<table>
<thead>
<tr>
<th>Antenna Parameters</th>
<th>Micro strip feed</th>
<th>Coaxial feed</th>
</tr>
</thead>
<tbody>
<tr>
<td>Types of feed</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Fractional Bandwidth</td>
<td>0.83%</td>
<td>1.29%</td>
</tr>
<tr>
<td>Return Loss (dB)</td>
<td>-30.7</td>
<td>-37.6</td>
</tr>
<tr>
<td>Gain (dBi)</td>
<td>6.732</td>
<td>7.157</td>
</tr>
<tr>
<td>Re (Impedance) @ 2.4GHz in Ω</td>
<td>50.9</td>
<td>51.4</td>
</tr>
<tr>
<td>Im (Impedance) @ 2.4GHz in Ω</td>
<td>2.084j</td>
<td>-0.29j</td>
</tr>
<tr>
<td>HPBW (deg.)</td>
<td>80</td>
<td>80</td>
</tr>
<tr>
<td>Radiation Efficiency</td>
<td>95.19%</td>
<td>99.04%</td>
</tr>
<tr>
<td>Polarization Purity</td>
<td>Poor</td>
<td>Poor</td>
</tr>
<tr>
<td>Spurious Radiation</td>
<td>More</td>
<td>More</td>
</tr>
</tbody>
</table>

As we got the result in HFSS tool of the simulated patch structure, we can say that this is a narrow band structure having impedance band width very small. We are getting the good return loss for an impedance bandwidth around 20 MHz. Gain of microstrip feed is 6.732 dBi whereas the gain of coaxial feed is 7.157 dBi. The Half power band width for both the cases is around 80°. The Radiation efficiency of patch is around 99% for the coax feed whereas 95% for the micro-strip feed patch structure. The magnitude of impedance is nearly 50 ohm hence we can say that this have a good impedance match with the SMA connector of 50 ohm impedance. The Polarization purity is poor and the Spurious radiation is high.

**REFERENCES**

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